## SHENZHEN DONGKE SEMICONDUCTOR CO., LTD PSR CONSTANT CURRENT I VOLTAGE IC-DK912

## SPECIFICATION

## 1. DESCRIPTION

The DK912 is a primary side flyback type AC-DC Switch Mode Power Controlling I C. It integrates 700 V high voltage power transistor and primary peak current detecting circuit. It also includes Primary Side Constant Current Regulation, Constant Voltage Control, Self-Power supply and Output cable compensation functions. And because of its highly integrated MOS circuit design, lots of external components are saved, transf ormer design is simple, only two windings are needed for the transformer in isolated output circuit.

## 2. APPLICATIONS

-Battery charger
-Power AC/DC adapters
-STB power supply
-Electromagnetic oven power supply
-DVD/VCD power supply

- Air conditioner power supply
-AC/DC LED driver applications
-TV/Monitor power supply


## 3. MAIN FEATURES

- Build-in 700 V high voltage power transistor.
$\cdot 85 \mathrm{~V}-265 \mathrm{~V}$ AC universal input range allows worldwide operation.
- Integrated high voltage constant current starting circuit, no need for additional starting resistance.
- Patent Primary Side Regulation control, no need for auxiliary winding.
- Patent self-power supply circuit design, no need for external winding power supply.
- Internal PMW oscillation circuit with Frequency jittering control to keep EMC characteristics.
- Over current, Over temperature, Over voltage and Short Circuit Protection.
$\cdot \pm 2 \%$ Voltage Accuracy, $\pm 5 \%$ Current Accuracy.
- 4KV Anti-Static ESD test.


## 4. POWER RANGE

| Input Voltage | $85-264 \mathrm{~V} \mathrm{AC}$ | $85-145 \mathrm{~V} \mathrm{AC}$ | $180-264 \mathrm{~V} \mathrm{AC}$ |
| :--- | :---: | :---: | :---: |
| MAX. output power | 12 W | 18 W | 18 W |

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## 5. CONNECTION DIAGRAM



PIN FUNCTION

| Pin NO. | Pin Name |  |
| :---: | :---: | :--- |
| 1 | IS | Current testing: 1. if IS connected to ground via resistor, Rs should be more <br> then $350 \mathrm{~m} \Omega$, Maximum Ip=Vlim/Rs; 2.if IS to ground directly, maximum <br> Ip=777mA |
| 2 | GND | Ground reference. |
| 3 | FB | Primary side feedback control pin. |
| 4 | VDD | Power supply pin. Connects a 10uF-47uF capacitor to ground. |
| $5,6,7,8$ | OC | Drain pin for internal high voltage power transistor. |

## 6. ABSOLUTE MAXIMUM RATINGS

| Parameter | Value | Unit |
| :--- | :--- | :--- |
| Supply voltage | $-0.3--8$ | V |
| Current of supply voltage | 100 | mA |
| Pin voltage | $-0.3--\mathrm{VDD}+0.3$ | V |
| Transistor withstand voltage | $-0.3--730$ | V |
| Peak current | 700 | mA |
| Total power dissipation | 1000 | mW |
| Operating temperature | $-25--+125$ | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature | $-55--+150$ | ${ }^{\circ} \mathrm{C}$ |
| Lead temperature | +280 | ${ }^{\circ} \mathrm{C} / 5 \mathrm{~S}$ |

## 7. ELECTRICAL CHARACTERISTIC

| Parameter | Condition | Value |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. |  |
| Power Supply voltage | AC input: $85 \mathrm{~V}-265 \mathrm{~V}$ | 4 | 4.7 | 6 | V |

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| Start threshold Voltage | AC input: 85V-265V | 4.5 | 4.7 | 5.0 | V |
| :--- | :--- | :---: | :---: | :---: | :--- |
| Restart Voltage | AC input: 85V-265V | 3.3 | 3.6 | 3.9 | V |
| Stop threshold Voltage | AC input: $85 \mathrm{~V}-265 \mathrm{~V}$ | 6 | 6.2 | 6.5 | V |
| Current of power | Vdd=5V, Fb=2V |  |  | 40 | mA |
| High voltage startup current | AC input: 265V |  |  | 0.5 | mA |
| Start time | AC input: 85 V | -- | -- | 500 | mS |
| BJT Breakdown voltage | Ioc $=1 \mathrm{~mA}$ | 700 |  |  | V |
| BJT Breakdown current | $\mathrm{Vdd}=5 \mathrm{~V}$ |  |  | 350 | mA |
| IS MAX. working voltage | $\mathrm{Vdd}=5 \mathrm{~V}$ | 360 | 400 | 440 | mV |
| IS MIN. working voltage | $\mathrm{Vdd}=5 \mathrm{~V}$ | 80 | 100 | 120 | mV |
| CV reference voltage | $\mathrm{Vdd}=5 \mathrm{~V}$ | 2.45 | 2.5 | 2.55 | V |
| Working frequency | $\mathrm{Vdd}=5 \mathrm{~V}$ | 16 k |  | 65 k | Hz |
| MIN startup time | $\mathrm{Vdd}=5 \mathrm{~V}$ |  | 500 |  | nS |
| Open circuit protection | $\mathrm{Vdd}=5 \mathrm{~V}, \mathrm{FB}$ voltage testing |  | 3.7 |  | V |
| Short circuit protection | $\mathrm{Vdd}=5 \mathrm{~V}$, FB voltage testing |  | 1.3 |  | V |
| Temperature protection | $\mathrm{Vdd}=5 \mathrm{~V}$ | 120 | 130 | 140 | ${ }^{\circ} \mathrm{C}$ |

## 8. OPERATION PRINCIPLE

### 8.1 Start Up

With its internal high voltage constant current driving circuit, external VDD capacitor would be charged when power on, when the voltage of VDD reaches 5 V , starting up process finished and the IC enters into soft start stage.

### 8.2 Soft Start

4 ms after starting up, the IC works at 16 khz , peak current is $\frac{1}{2} * \operatorname{Ip}$ max
1 mS after starting up delayed, begins to detect FB voltage

### 8.3 FB detecting

In the flyback stage, output voltage was mapped to FB pin via the Coupling relationship of primary side or secondary side winding. IC detects and controls the output current and voltage via detecting the FB voltage. When it detects the $\mathrm{FB}>0.7 \mathrm{~V}$, it would judge flyback beginning and sample the FB voltage. As to avoid mistakes of taking the leakage voltage, it would begin sampling 2.5 us later. The sampled voltage of FB would be compared with the internal reference voltage of 2.5 V , error amplifier controls the primary peak current Ip with its output control, so that to adjust output voltage and current.

### 8.4 Constant Current output control

When loading is more then its maximum output power, output voltage decreases, FB's voltage is less tehn

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2.5 V , IC will work at constant current status. Output current $I o \approx \frac{1}{4} * I p \max * N$. Working frequency $F s=\frac{N * \text { Vout }}{2 * L p^{*} I p \max }$. As per the loading keep on increasing, output voltage decreases and the Fs decreases.

### 8.5 Constant Voltage output control

When the loading is less then its maximum output power, IC will work at constant voltage status, if will control the peak current and working frequency accordingly loading status. When heavy loaded, working frequency is fixed on 65 khz , IC works at PWM mode. While loading decreases, Ip decreases accordingly. When it enters light loadings, Fs decreases from 65 khz to 20 khz , IC works at PFM mode. If loading keeps on decreasing or to empty load, IC enters into jump off mode so that to keep low power consumption.
As per below typical application sample:

When using in two winding CV application:

$$
V_{\text {OUT }} \approx \frac{2.5 v^{*} N s}{N_{\mathrm{p}}} *\left(1+\frac{R F B 2}{R F B 1}\right)-V_{d}
$$

$$
V_{\text {OUT }} \approx \frac{2.5 v^{*} N s}{N_{A}} *\left(1+\frac{R F B 2}{R F B 1}\right)-V_{d}
$$

( Vd is the voltage of the secondary current rectifier diode)

### 8.6 Peak Current Protection

Ris ( resistor connected with PIN IS to ground) is resistor of current sampling, if is used for setting the maximum output power of the power supply. Because Vin*Von=Lp*Ip, so as to make sure of high output power, when input voltage is low, Vin $=100 \mathrm{~V}$, startup time Ton's maximum value is 8us. Also $P o \max =\frac{1}{2} L p^{*} I p \max ^{2} * F s \max ^{*} \eta, \quad I_{\mathrm{p}}=\frac{2^{*} P_{o} \max }{V_{\mathrm{IN}}{ }^{*} T_{\mathrm{ON}} * F s \max ^{*} \eta}, \quad L_{P}=\frac{2^{*} P o \max }{I_{P}^{2} * F s \max { }^{*} \eta}$
( $\eta$ is the efficiency of the power supply)

### 8.7 Self-Power Supply Circuit (National patent owned)

There is self-power supply circuit inside the IC, which can control the VDD voltage at about 4.7 V for the electricity consumption of the IC itself. So that can save external winding power supply.

### 8.8 Cable compensation

With Cable compensation circuit, can decrease the output voltage error caused by cable resistance in different loading. Cable compensation current Icomp increases when loading increases, maximum value is 12 uA .

For three windingly application, cable compensation voltage is $2 * \frac{N_{\mathrm{S}}}{N_{\mathrm{A}}} * I_{\mathrm{COMP}} * R_{\mathrm{FB} 2}$
For two windingly application, cable compensation voltage is $2 * \frac{N_{\mathrm{S}}}{N_{\mathrm{P}}} * I_{\mathrm{COMP}} * R_{\mathrm{FB} 2}$

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### 8.9 Abnormal Voltage Protection

Whenever the power voltage (Vcc) abnormally exceeds 6.2 V , the controller would stop operation and enters into stop status.

### 8.10 Abnormal FB voltage Protection

If secondary side is of open circuit, Vor keeps on increasing. When FB pin's detected voltage is more then 3.7 V , the IC enters into protection status.

After power on, if FB resistor is detected to be disconnected, IC will enter into protection status.

### 8.11 Transistor Over Voltage Protection

Whenever more then 600 V is detected on the power transistor, IC will enter into protection status.

### 8.12 Short Circuit Protection

As to protect the secondary side, whenever the lower then 1.3 V is detected on FB and lasting time is more then 8 ms , IC will enter into protection status.

### 8.13 Over Temperature Protection (OTP)

When the controller detects the IC temperature exceeds $130^{\circ} \mathrm{C}$, OTP is activated. It stops the switching operation immediately and enters into the stop status. The controller will restart to switching operation when the temperature falls down.

## 9. TYPICAL APPLICATION SAMPLE 1

## 5V 2A with two winding wires


9.1 Components list

| NO. | NAME | SPEC. / MODEL NO. | POSITION | USED QTY | REMARK |
| :--- | :--- | :---: | :---: | :---: | :---: |
| 1 | Fuse | F1A/AC250V | F1 | 1 |  |
| 2 | rectifier | 1N4007 | D1 $^{\text {DD }} 4$ | 4 |  |
| 3 | Diode | FR107 | D5 | 1 |  |
| 4 | Diode | SR540 | D6 | 1 |  |

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| 5 | Electrolytic capacitor | $10 \mathrm{uF} / 400 \mathrm{~V}$ | $\mathrm{C} 1, \mathrm{C} 2$ | 2 |  |
| :--- | :--- | :---: | :---: | :---: | :--- |
| 6 | Electrolytic capacitor | $10 \mathrm{uF} / 16 \mathrm{~V}$ | C 3 | 1 |  |
| 7 | Electrolytic capacitor | $1000 \mathrm{uF} / 10 \mathrm{~V}$ | C 5 | 1 |  |
| 8 | Electrolytic capacitor | $470 \mathrm{uF} / 10 \mathrm{~V}$ | C 6 | 1 |  |
| 9 | Inductor | $1 \mathrm{mH} / \mathrm{EMI}$ | L 1 | 1 |  |
| 10 | Inductor | $10 \mathrm{uH} / 2.5 \mathrm{~A}$ | L 2 | 1 |  |
| 11 | Ceramic capacitor | 2 A 103 J | C 4 | 1 |  |
| 12 | Ceramic capacitor | Y capacitor 102 | C 7 | 1 |  |
| 13 | Ceramic capacitor | DN1 | C 8 | 1 |  |
| 14 | Resistance | 150 K | R 1 | 1 | $1 \%$ accuracy |
| 15 | Resistance | $47 \Omega$ | R 2 | 1 | $1 \%$ accuracy |
| 16 | Resistance | $0.56 / 0.5 \mathrm{~W}$ | RS | 1 | $1 \%$ accuracy |
| 17 | Resistance | 250 K | RFB 2 | 1 | $1 \%$ accuracy |
| 18 | Resistance | 8 K | RFB 1 | 1 | $1 \%$ accuracy |
| 19 | IC | DK912 | U 1 | 1 |  |
| 20 | Transformer | EE19 | T1 | 1 |  |

### 9.2 TRANSFORMER DESIGN

### 9.2.1 Parameter confirmation: confirm the below parameter before transformer design

(1) Input voltage range:AC85V-265V
(2) Output Voltage and current: for example DC5V 2A, MAX. switch mode frequency: 65 khz , MAX. duty cycle: $50 \%$

### 9.2.2 Core selecting

(1) Input power calculation
$\mathrm{P}=$ Pout $/ \eta \quad(\eta$ is the efficiency of the power supply, take it 0.75 for example), Pout=Vout*lout $=5 \mathrm{~V}^{*} 2 \mathrm{~A}=10 \mathrm{~W}$, so $\mathrm{P}_{\text {in }}=10 / 0.75=13.3 \mathrm{~W}$.
(2) Choose the core:

Checking via supplier or the correlative chart can know that EE19 core is suitable for 13.3 W power supply. And $\mathrm{Ae}=23 \mathrm{~mm}^{2}$

### 9.2.3 Turn ratio of transformer

Flyback voltage of transformer $\left(\mathrm{V}_{\text {or }}\right)$ is normally set to be $60 \mathrm{~V}-120 \mathrm{~V}$, and 80 V is recommended normally.
$N=\frac{\text { Vor }}{\text { Vout }}=\frac{80 \mathrm{~V}}{5.5 \mathrm{~V}} \approx 15$

### 9.2.4 Resistor Rs calculation

As mentioned above,

$$
I_{\mathrm{P}}=\frac{2 * \operatorname{Po} \text { max }}{V_{\mathrm{IN}} * T_{\mathrm{nN}} * F s \max ^{*} \eta}=\frac{2 * 10 \mathrm{~W}}{100 \mathrm{~V}^{*} 8 u s^{*} 60 \mathrm{~K}^{*} 0.75} \approx 560 \mathrm{~mA},
$$

$I p \max =\frac{400 \mathrm{mv}}{R s+0.1} \quad \Rightarrow \quad R s \approx 0.6 \mathrm{ohm}$,
in actual testing, we take $\mathrm{RS} \approx 0.56 \mathrm{hm}$, so that output is 10 W .

### 9.2.5 Inductor calculation

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$$
P_{\text {in }}=\frac{1}{2} L^{*} I_{\mathrm{P}}^{2} * F s, \quad L=\frac{2 * P o \max }{I_{\mathrm{P}}^{2} * F s \max * \eta}=\frac{2 * 10 \mathrm{~W}}{0.56 A^{2} * 60 K^{*} 0.75} \approx 1.4 \mathrm{mH}
$$

### 9.2.6 Number of the original(input) turns ( $\mathbf{N p}$ )

$$
\lambda=N_{\mathrm{P}} * A_{\mathrm{e}} * B, \quad \lambda=L * I_{\mathrm{P}}, \text { so } \quad N_{\mathrm{P}}=\frac{L^{*} I_{\mathrm{P}}}{B^{*} A_{\mathrm{e}}}
$$

Because the saturation magnetization of Ferrite material is about 0.4 T , the designed Magnetic flux density in transformer should be no more then 0.4T. However, Single-ended Flyback circuits works in the first quadrant of $\mathrm{B}-\mathrm{H}$, and residual magnetism of the core is about 0.1 T , so the maximum working magnetic flux density should be $0.4-0.1=0.3 \mathrm{~T}$. According to formula $\mathrm{Bmax}=\left(I_{p} * L_{p}\right) /\left(N_{p} * A_{e}\right)=0.3 T$, here below takes 0.25 T for calculation, and $\mathrm{A}_{\mathrm{e}}$ in EE19 transformer is $23 \mathrm{~mm}^{2}$, so we can get that
$N_{p}=I_{p} * L_{p} / \mathrm{B} \max * A e=560 m A * 1.4 m H\left(/ 0.25 T^{*} 23 \mathrm{~mm}^{2}\right) \approx 136$
We take 136 turns in actual use.

### 9.2.7 Number of the output turns (Ns)

$$
N_{s}=N_{p} / N=135 / 15=9
$$

### 9.2.8 Leakage inductance of a transformer

It is suggested to use $\mathrm{P} / \mathrm{S} / \mathrm{P}$ way to wind the transformer so that to reduce the leakage inductance.

## 10. TYPICAL APPLICATION SAMPLE 2

5V 2A with three winding wires


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### 10.1 Components list

| NO. | NAME | SPEC. / MODEL NO. | POSITION | USED QTY | REMARK |
| :--- | :--- | :--- | :---: | :---: | :---: |
| 1 | Fuse | F1A/AC250V | F 1 | 1 |  |
| 2 | Diode | 1 N 4007 | $\mathrm{D} 1^{\sim} \mathrm{D} 4$ | 4 |  |
| 3 | Diode | 1 N 4007 | D 5 | 1 |  |
| 4 | Diode | SR540 | D 6 | 1 |  |
| 5 | Electrolytic capacitor | $10 \mathrm{uF} / 400 \mathrm{~V}$ | $\mathrm{C} 1, \mathrm{C} 2$ | 2 |  |
| 6 | Electrolytic capacitor | $10 \mathrm{uF} / 16 \mathrm{~V}$ | C 4 | 1 |  |
| 7 | Electrolytic capacitor | $1000 \mathrm{uF} / 16 \mathrm{~V}$ | C 5 | 1 |  |
| 8 | Electrolytic capacitor | $470 \mathrm{uF} / 16 \mathrm{~V}$ | C 6 | 1 |  |
| 9 | Inductor | $1 \mathrm{mH} / \mathrm{EMI}$ | L 1 | 1 |  |
| 10 | Inductor | $10 \mathrm{uH} / 2.5 \mathrm{~A}$ | L 2 | 1 |  |
| 11 | Ceramic capacitor | 2 A 103 J | C 3 | 1 |  |
| 12 | Ceramic capacitor | Y capacitor 102 | C 7 |  |  |
| 13 | Ceramic capacitor | DN1 | C 8 |  |  |
| 14 | Resistance | 150 K | R 1 | 1 | $1 \%$ accuracy |
| 15 | Resistance | $47 \Omega$ | R 2 | 1 | $1 \%$ accuracy |
| 16 | Resistance | $0.56 / 0.5 \mathrm{~W}$ | RS | 1 | $1 \%$ accuracy |
| 17 | Resistance | 10 K | RFB 2 | 1 | $1 \%$ accuracy |
| 18 | Resistance | 8.2 K | RFB1 | 1 | $1 \%$ accuracy |
| 19 | IC | U1 | 1 |  |  |
| 20 | Transformer | EE19 | T1 | 1 |  |

### 10.2 TRANSFORMER DESIGN

### 10.2.1 Parameter confirmation: confirm the below parameter before transformer design

(1) Input voltage range:AC85V-265V
(2) Output Voltage and current: for example DC5V 2A, MAX. switch mode frequency: 65khz, MAX. duty cycle: 50\%

### 10.2.2 Core selecting

(1) Input power calculation
$\mathrm{P}=$ Pout $/ \eta \quad(\eta$ is the efficiency of the power supply, take it 0.75 for example), Pout $=$ Vout $*$ lout $=5 \mathrm{~V} * 2 \mathrm{~A}=5 \mathrm{~W}$, so $\mathrm{P}_{\text {in }}=10 / 0.75=13.3 \mathrm{~W}$.
(2) Choose the core:

Checking via supplier or the correlative chart can know that EE19core is suitable for 13.3 W power supply. And $\mathrm{Ae}=23 \mathrm{~mm}^{2}$

### 10.2.3 Turn ratio of transformer

Flyback voltage of transformer $\left(\mathrm{V}_{\text {or }}\right)$ is normally set to be $60 \mathrm{~V}-120 \mathrm{~V}$, and 80 V is recommended normally.
$N=\frac{\text { Vor }}{\text { Vout }}=\frac{80 \mathrm{~V}}{5.5 \mathrm{~V}} \approx 15$

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### 10.2.4 Resistor Rs calculation

As mentioned above, $I_{\mathrm{P}}=\frac{2^{*} P o \max }{V_{\mathrm{rv}}^{*} T_{\mathrm{nN}} * F s \max ^{*} \eta}=\frac{2 * 10 \mathrm{~W}}{100 \mathrm{~V}^{*} 8 u s^{*} 60 \mathrm{~K}^{*} 0.75} \approx 560 \mathrm{~mA}$, $I p \max =\frac{400 \mathrm{mv}}{R s+0.1} \quad \Rightarrow \quad R s \approx 0.6 \mathrm{ohm}$, in actual testing, we take $\mathrm{RS} \approx 0.56 \mathrm{ohm}$, so that output is 10 W .

### 10.2.5 Inductor calculation

$$
P_{\mathrm{in}}=\frac{1}{2} L * I_{\mathrm{P}}^{2} * F s, \quad L=\frac{2 * \text { Po } \max }{I_{\mathrm{P}}^{2} * F s \max * \eta}=\frac{2 * 10 \mathrm{~W}}{0.56 A^{2} * 60 K^{*} 0.75} \approx 1.4 \mathrm{mH}
$$

### 10.2.6 Number of the original(input) turns (Np)

$$
\lambda=N_{\mathrm{P}} * A_{\mathrm{e}} * B, \quad \lambda=L * I_{\mathrm{P}}, \text { so } \quad N_{\mathrm{P}}=\frac{L^{*} I_{\mathrm{P}}}{B^{*} A_{\mathrm{e}}}
$$

Because the saturation magnetization of Ferrite material is about 0.4 T , the designed Magnetic flux density in transformer should be no more then 0.4 T . However, Single-ended Flyback circuits works in the first quadrant of $\mathrm{B}-\mathrm{H}$, and residual magnetism of the core is about 0.1 T , so the maximum working magnetic flux density should be $0.4-0.1=0.3 \mathrm{~T}$. According to formula $\mathrm{Bmax}=\left(I_{p}{ }^{*} L_{p}\right) /\left(N_{p} * A_{e}\right)=0.3 T$, here below takes 0.25 T for calculation, and $\mathrm{A}_{\mathrm{e}}$ in EE19 transformer is $23 \mathrm{~mm}^{2}$, so we can get that
$N_{p}=I_{p} * L_{p} / B_{\max } * A e=560 m A * 1.4 m H\left(/ 0.25 T^{*} 23 \mathrm{~mm}^{2}\right) \approx 136$
We take 135turns in actual use.

### 10.2.7 Number of the output turns (Ns)

$$
N_{s}=N_{p} / N=135 / 15=9
$$

Auxiliary winding should be of same terns as secondary winding turns, and next to secondary winding.

### 10.2.8 Leakage inductance of a transformer

It is suggested to use $\mathrm{P} / \mathrm{S} / \mathrm{P}$ way to wind the transformer so that to reduce the leakage inductance.

## 11. SPECIAL NOTICE FOR PBC LAYOUT DESIGN

11.1 The main heat dissipation is from transistor of the IC, and it is connected with the OC pin. So enough cooper area connected to the OC pin and tin-plating are necessary to provide the controller heat sink.
11.2 The OC pin is high voltage part of the IC, peak voltage is as high as 600 V , so it should be at least 1.5 mm far away from the low voltage part in the PCB as to avoid circuit breakdown and discharging.
11.3 The self-power supply circuit in IC works in high frequency situation, too long or too thin cable would cause abnormal working of the IC, so the capacitor connected to pin No. 4 should be near to IC and the cable area should be enlarged.

## 12. MECHANICAL AND PACKING INFORMATION

| Symbol | Dimensions In Willimeters |  | Dimensions In Inches |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Min | Nax | Win | Nax |
| A | 3.710 | 4.310 | 0.146 | 0.170 |
| A1 | 0.510 |  | 0.020 |  |
| A2 | 3. 200 | 3.600 | 0.126 | 0.142 |
| B | 0.380 | 0.570 | 0.015 | 0.022 |
| B1 | 1.524(BSC) |  | 0.060 (BSC) |  |
| C | 0.204 | 0.360 | 0.008 | 0.014 |
| D | 9.000 | 9.400 | 0.354 | 0.370 |
| E | 6. 200 | 6.600 | 0.244 | 0.260 |
| E1 | 7.320 | 7.920 | 0.288 | 0.312 |
| e | 2.540 (BSC) |  | 0.100 (BSC) |  |
| L | 3.000 | 3.600 | 0.118 | 0.142 |
| E2 | 8.400 | 9.000 | 0.331 | 0.354 |



- Packing quantity

| QTY/tube | QTY/inner carton | QTY/master carton |
| :---: | :---: | :---: |
| 50 | 2000 | 20000 |

